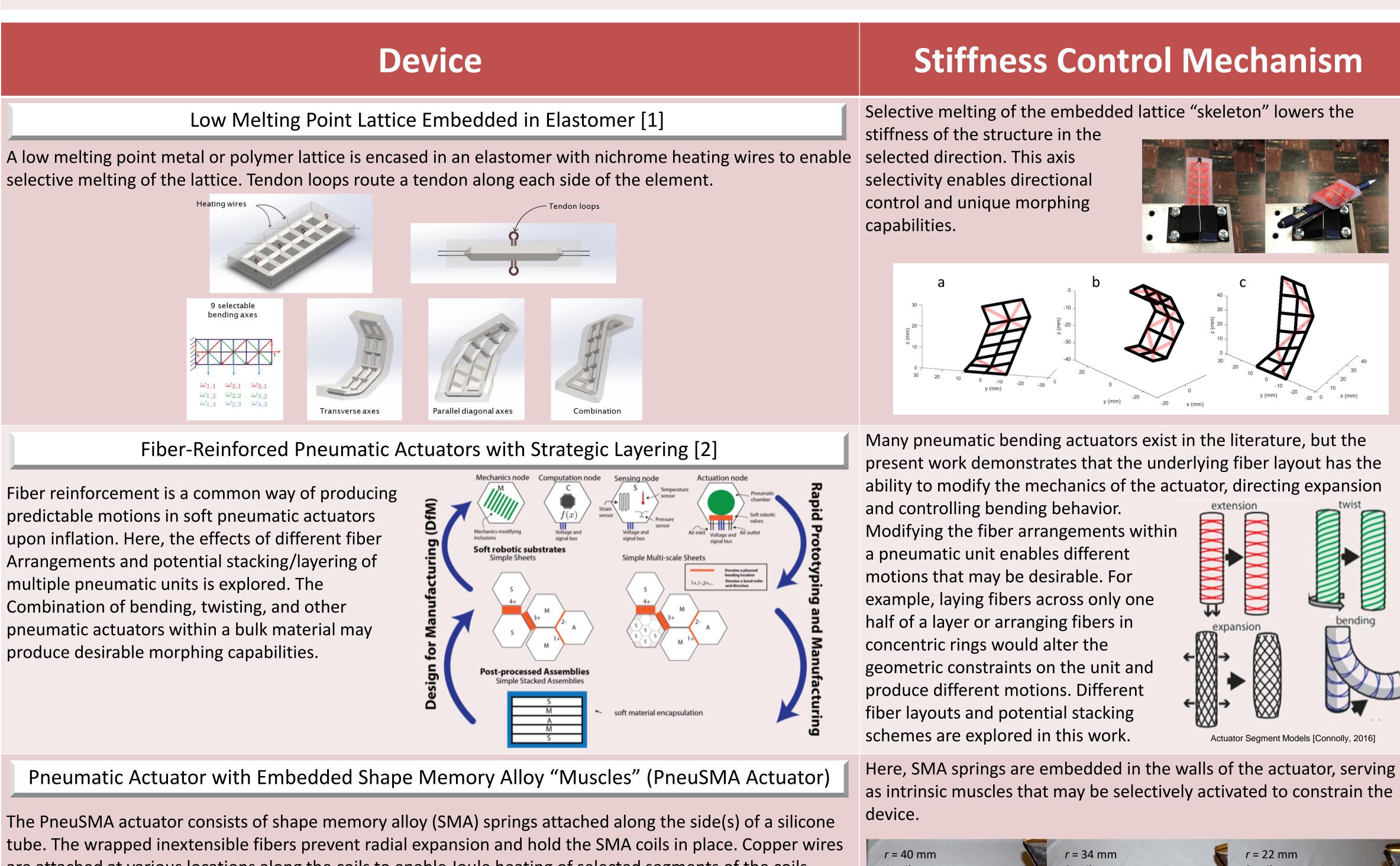
Directional Stiffness Control of Soft Robotics Materials

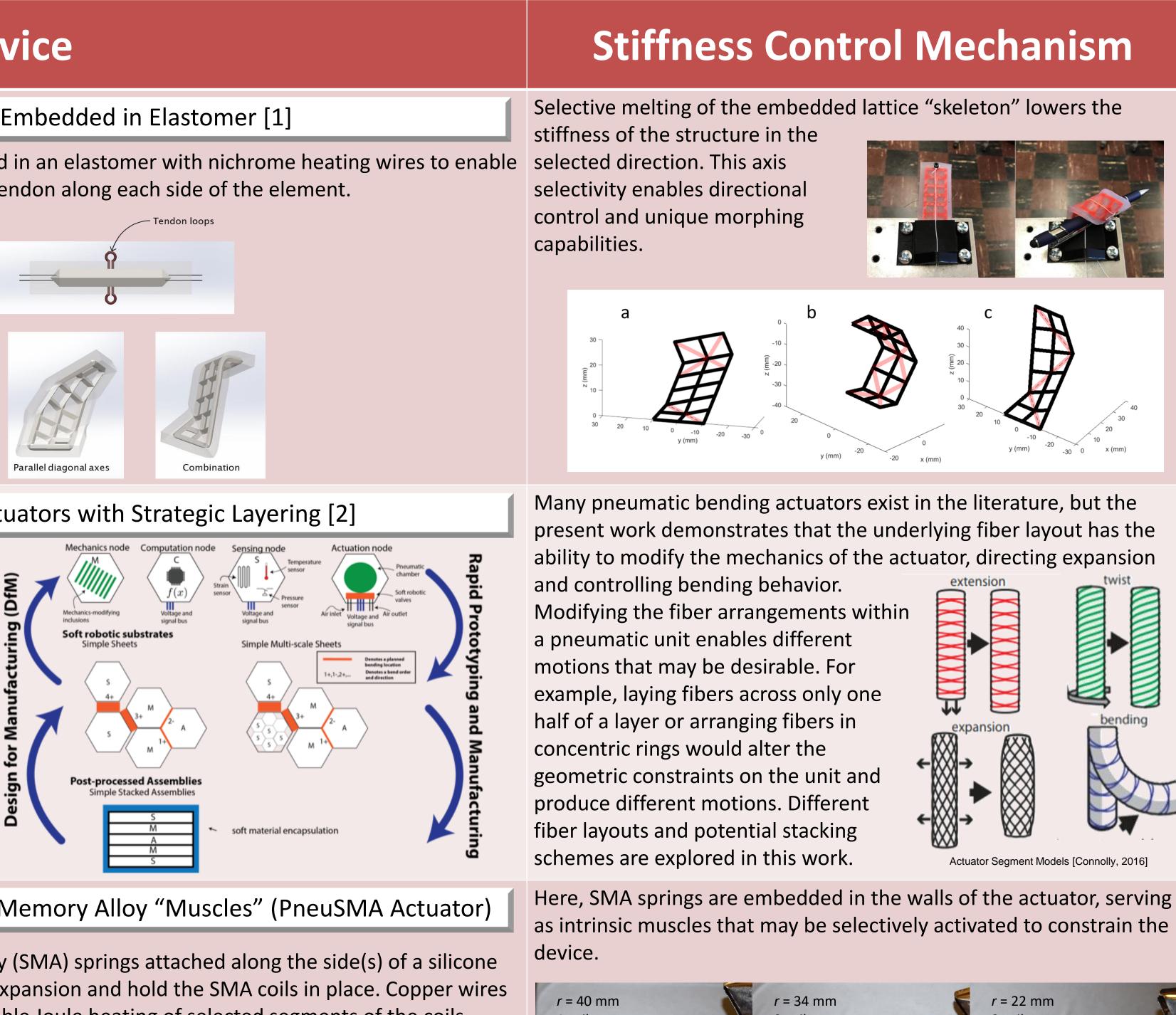


https://labs.wsu.edu/m3robotics/

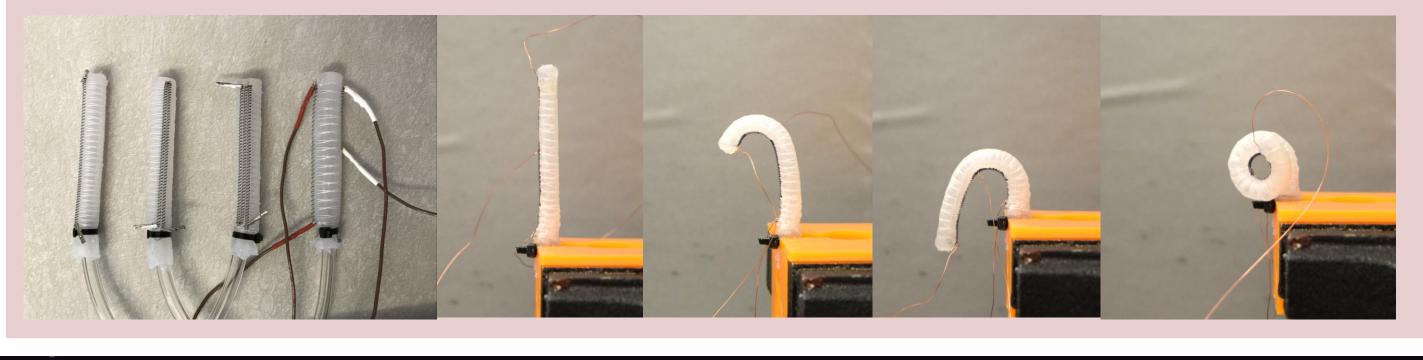
References [1] E. A. Allen, B. C. Townsend, and J. P. Swensen, "Configuration Modeling of a Soft Robotic Element with Selectable Bending Axes," in Proc. IEEE/RSJ International Conference on Intelligent Robots and Systems (IROS2019), Macau, China, Nov. 2019. [2] E. A. Allen and J. P. Swensen, "Versatile Layering Approach to Pneumatic Soft Actuator Fabrication," in Proc. ASME 2019 Conference

Summary and Motivation Traditionally, robotic systems have followed the paradigm of being comprised primarily of rigid structures with relatively few degrees of freedom and well-characterized motion driven by actuators directly connected to the rigid links. In recent years, there has been an explosion of research in the area of soft robotics, as they provide the promise of allowing robots and humans to work and collaborate in the same workspace. However, soft robotics have inherently limited ability to exert forces and interact with their surroundings in a meaningful way because of their compliant nature. Hence there is a great need for materials and mechanisms that can dynamically change between acting as a soft or a rigid robotic component. This work focuses on the directional control of stiffness within soft robotics materials. on Smart Materials, Adaptive Structures and Intelligent Systems (SMASIS2019), Louisville, KY, 2019, p. V001T01A001.





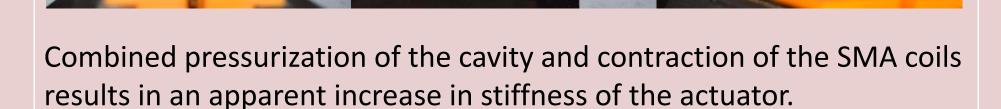
are attached at various locations along the coils to enable Joule heating of selected segments of the coils.



2020 National Robotics Initiative (NRI) Principal Investigators' Meeting FEBRUARY 27 - 28, 2020 | ARLINGTON, VIRGINIA

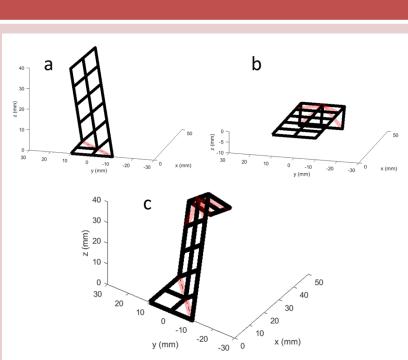
Washington State University | M3 Robotics Laboratory | Dr. John Swensen

1 coil 2 coils 3 coils



Mode of Actuation

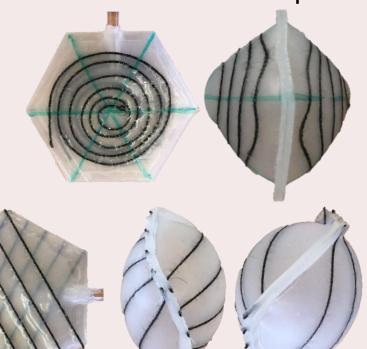
With the axis Selectivity enabled by Localized Heating elements, a single tendon on each side of the



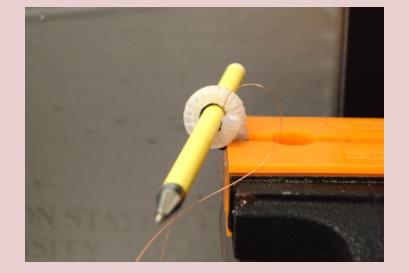
element activates a variety of unique configurations, especially when axes are allowed to cool and re-solidify in a new configuration before activating the next axis.

Similar to examples seen in nature such as a Venus flytrap plant and the muscular hydrostats, here the combination of hydrostatic pressure and constraints imposed by inextensible

fibers creates unique bending Behavior.



The PneuSMA actuator is controlled via activation of different SMA springs within the actuator, in conjunction with pneumatic actuation. The actuator demonstrates remarkable spatial controllability evidenced by testing under different pressures and SMA activation combinations.

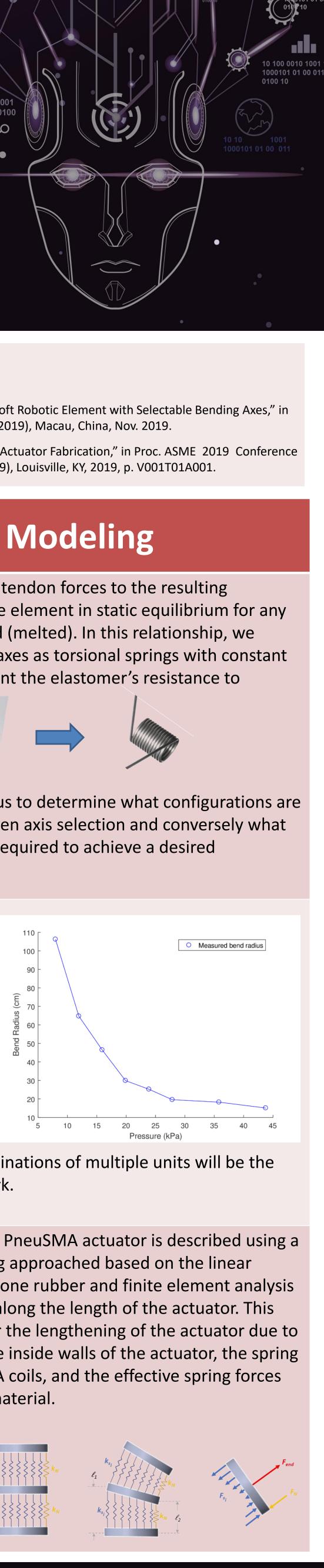


Here we relate the tendon forces to the resulting configuration of the element in static equilibrium for any set of axes selected (melted). In this relationship, we model the melted axes as torsional springs with constant stiffness to represent the elastomer's resistance to bending.

This model allows us to determine what configurations are possible for any given axis selection and conversely what tendon forces are required to achieve a desired configuration.

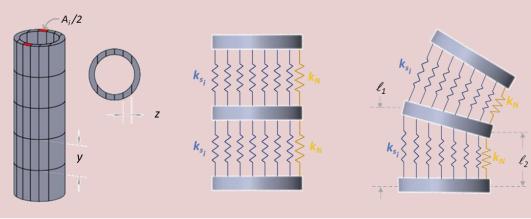
Experimental

measurements of a simple bending module are shown on the right. Developing a model to describe the bending and twisting behavior of the different



modules and combinations of multiple units will be the focus of future work.

The bending of the PneuSMA actuator is described using a simplified modeling approached based on the linear stiffness of the silicone rubber and finite element analysis of parallel springs along the length of the actuator. This model accounts for the lengthening of the actuator due to the pressure on the inside walls of the actuator, the spring force from the SMA coils, and the effective spring forces from the silicone material.



Award ID#: 1734117