

NRI: Shape Morphing Arm Robotic (SMART) Manipulators for Simultaneous Safe Human-Robot Interaction and High Performance in Manufacturing

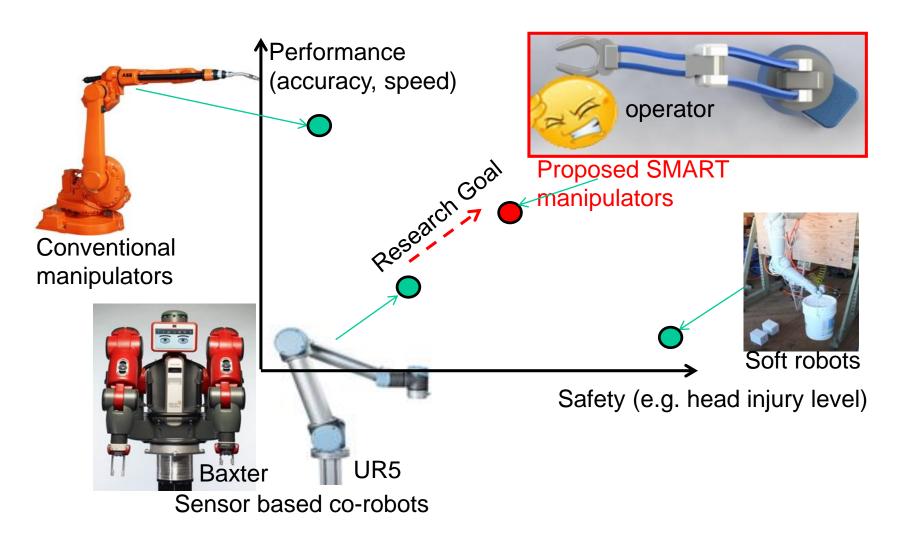
(NSF CMMI-1637656, 09/01/2016-08/31/2019)

Hai-Jun Su (PI), Marcelo Dapino
Department of Mechanical and Aerospace Engineering
The Ohio State University
Junmin Wang, University of Texas, Austin

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Motivations and Research Goals

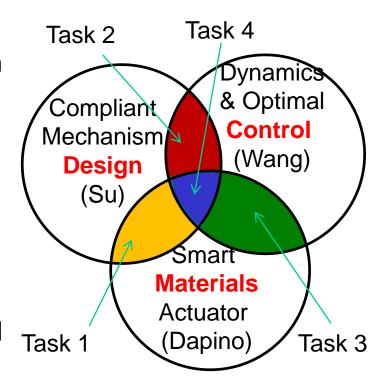
- Conventional: design for performance, safety by control
- Objective: safety by design, performance by control



Research Team and Tasks

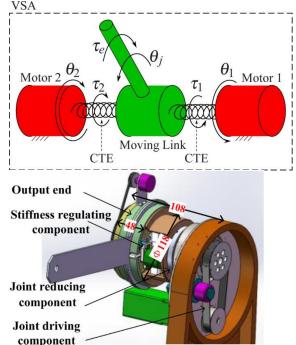
Research Tasks

- TASK 1: Develop a compliant mechanism and smart material actuator co-design framework for SMART links (Su, Dapino)
- TASK 2: Develop a control law and compliant mechanism co-design framework of SMART links with safety constraints (Su, Wang)
- TASK 3: Investigate methods for simultaneously controlling link motion and stiffness for achieving maximum performance under HIC constraint (Wang, Dapino)
- TASK 4: Integrate a comprehensive compliance design, stiffness modulation, and motion control framework of multilinked SMART manipulators (Su, Dapino, Wang)

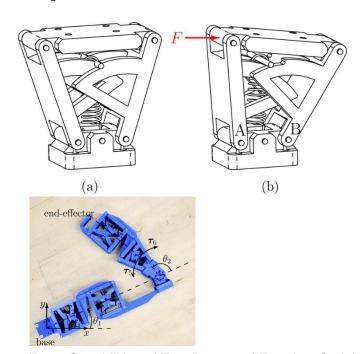


Current Solutions of Corobots

- Sensor based: vision for collision detection, torque/force sensor at joints
- Variable stiffness actuators (VSA): series elastic actuators/joints
- Mechanical Fuse: maximum force/torque limit



Design of Variable Stiffness Actuator Based on Modified Gear–Rack Mechanism, Wang et al., ASME JMR, 2016.

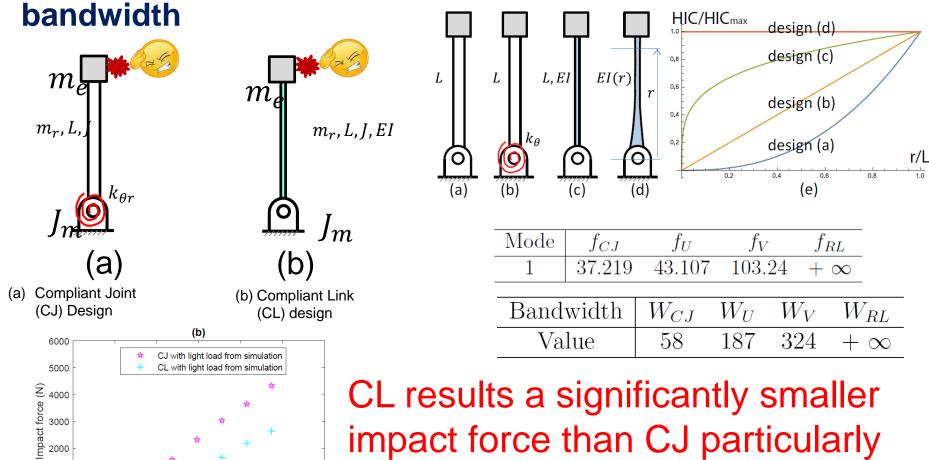


Force Capabilities of Two-Degree-of-Freedom Serial Robots Equipped With Passive Isotropic Force Limiters, Zhang et al., ASME JMR, 2016

Comparison of Compliant Link and Compliant Joints

Compare safety criteria: HIC distribution/impact force

Compare the control performance: natural frequency and



1000

0.5

1.5

Impact velocity (m/s)

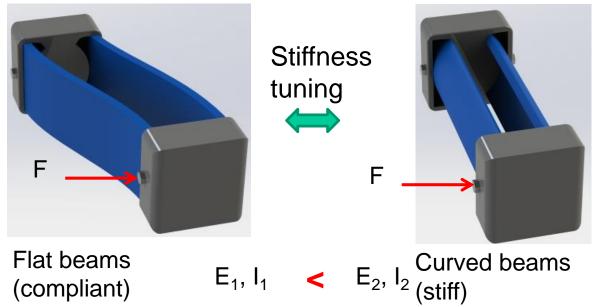
2.5

3

CL results a significantly smaller impact force than CJ particularly for small m_e/m_r .

The Design Strategy for Variable Stiffness Links

 Variable stiffness of compliant links via shape morphing, material property tuning



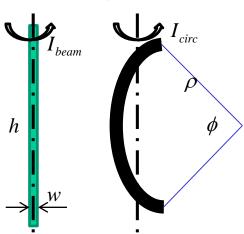
 Head Injury Criterion (HIC) is determined by mass, velocity and stiffness

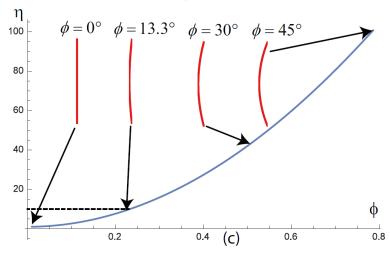
HIC = 1.016
$$T$$
 $\left(k_{eff}^{0.75}\right) \left(\frac{m_{oper}^{-0.75} m_{eff}^{1.75}}{(m_{eff} + m_{oper})^{1.75}}\right) \left(v^{2.5}\right)$

Variable Stiffness via Shape Morphing

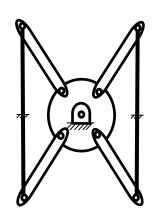
- Moment of inertia of straight beam vs. curved beams
- Shape morphing actuation via four-bar linkages

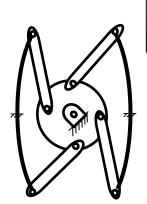
Concept Design

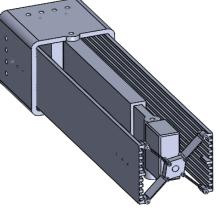


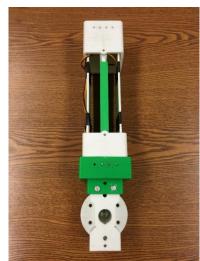


Hardware Implementation









Impact Testing Results

Head Injury Criteria (HIC)

$$HIC(\Delta t_{max}) = \max_{\Delta t} \left\{ \Delta t \left[\frac{1}{\Delta t} \int_{t_1}^{t_2} \hat{a} dt \right]^{2.5} \right\}$$

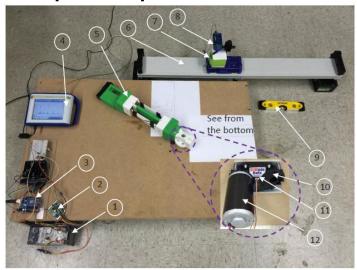
Actual stiffness change ratio ≈ 3.6

subject to
$$\Delta t = t_2 - t_1 \le \Delta t_{max}$$

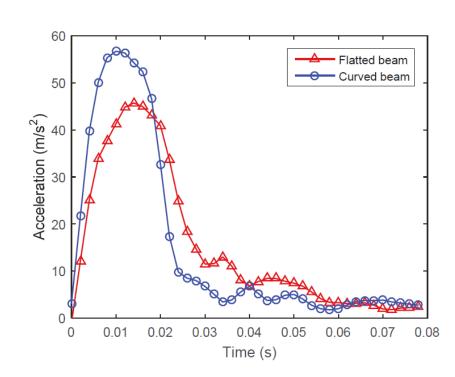
- Impact testing results:
 - Peak acceleration dropped from 56.7 m/s² to 45.7 m/s²

-29% (210.3 m^{2.5}/s⁻⁴ to 153.3 m^{2.5}/s⁻⁴) reduction in HIC at

impact speed of 2.2m/s

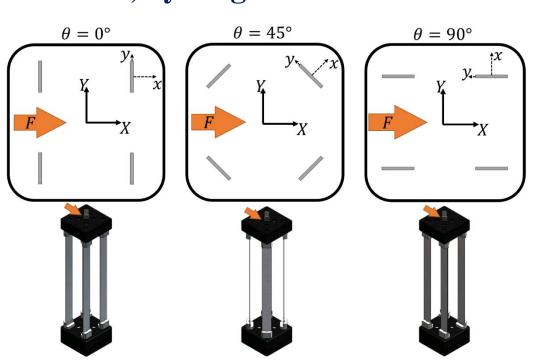


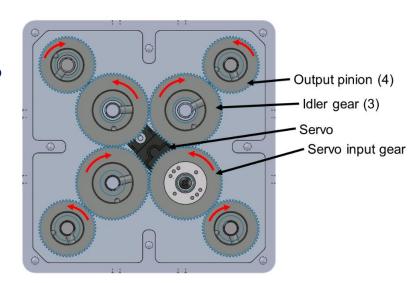
 Power supply, 2. Speed controller, 3. Micro-controller, 4. PASCO PS-2008A, 5. Morphing arm, 6. PAStrack Dynamics System ME-6962, 7. Force sensor, 8. Acceleration sensor, 9. Stanley Level, 10. Gear box, 11. Encoder, 12. DC motor

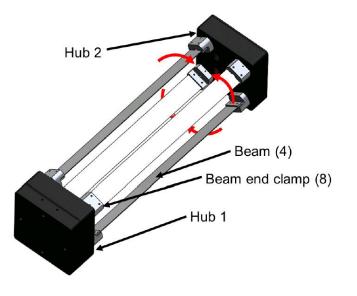


Variable Stiffness by Rotating Beams

- Synchronized symmetric beams change the second moment of inertia, so that $I(\theta)$ in $k = n \frac{EI}{L^3}$
- Aluminum beams, small hobby servos, nylon gears





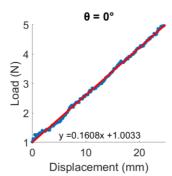


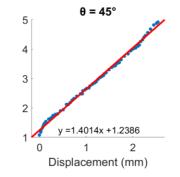
Testing Results

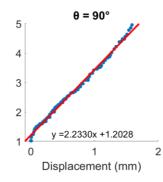
- Stiffness ratio ≈ 13.9
- **Analytical model from first** principles accounts for buckling & actuation components predicts stiffness variation.

•
$$k(\theta) = \frac{k_x + k_y}{2} + \frac{k_x - k_y}{2} \cos(2\theta)$$

Load vs Displacement Measurement of Stiffness







Max stiffness: 2.25 N/mm

Min stiffness: 0.16 N/mm

Median stiffness: 1.38 N/mm

Max/min stiffness ratio: 13.9

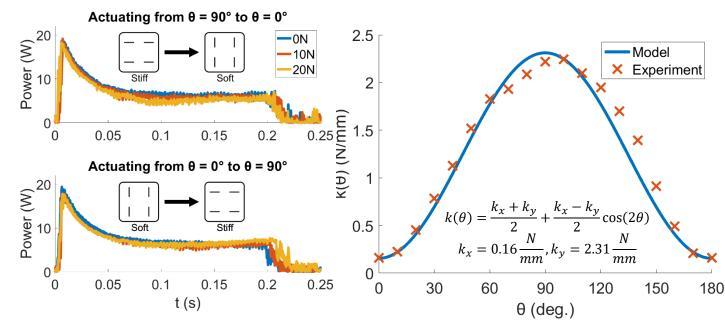
Actuation time: <0.25 s

Peak power draw: 15 W

Average power draw: 9 W

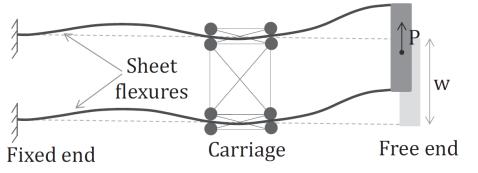
Mass of Design: 1.27 kg

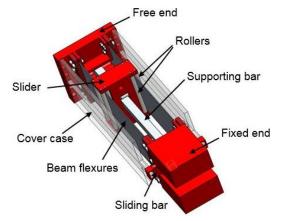
Comparison of Stiffness With Model Power Consumption Actuating Under Load

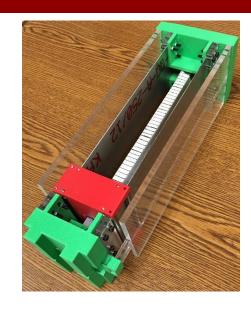


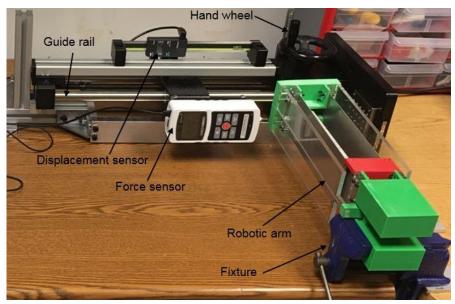
Variable Stiffness by Changing Effective Length

- Change effective length in $k \propto \frac{EI}{L^3}$
 - L ranged from 5 to 30 cm.
 - k change from 4.2×10^3 to 193 N/m, about 21.7 fold.
- Drive carriage by lead screw with DC motor or pneumatic linear actuator.



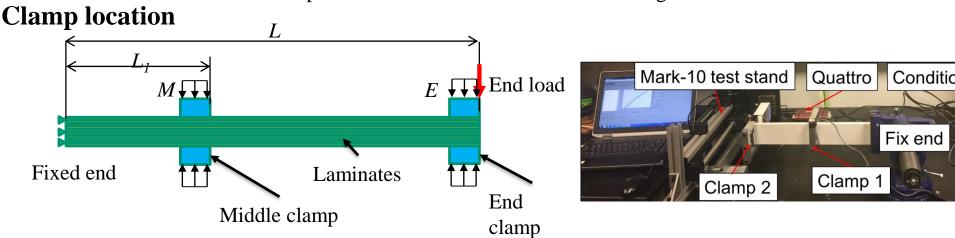






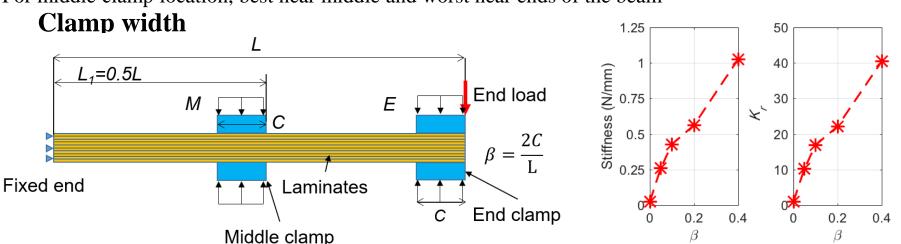
Discrete Layer Jamming Concept (1)

Key Parameters: clamp location, clamp width, friction coefficient, number of clamps, and number of laminates Stiffness is obtained from force-displacement curves from cantilever bending simulation



Both stiffness and stiffness ratio have maximum values at $\alpha = 0.5$, i.e. $L_1 = 0.5L$

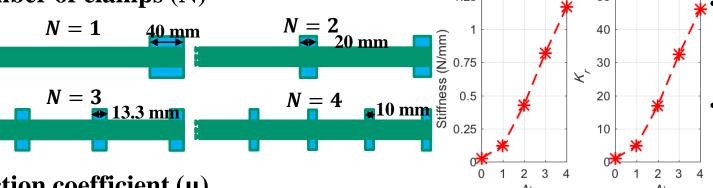
For middle clamp location, best near middle and worst near ends of the beam



Stiffness increases with clamp width, a 40.4 times stiffness change can be achieved with 40% of the area of the beam clamped Large, stiff clamps can add bulk to the system

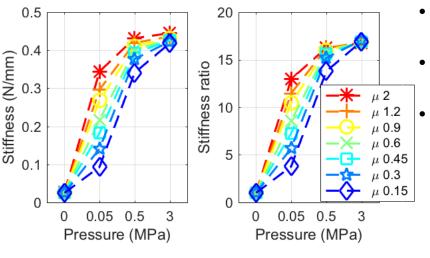
Discrete Layer Jamming Concept (2)





The more clamps, the higher the stiffness and stiffness ratio 4 clamps yield a maximum stiffness ratio of 46

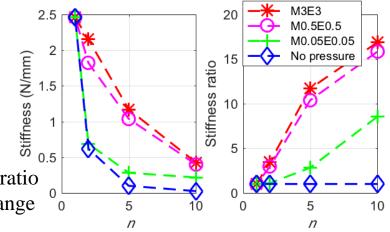
Friction coefficient (µ)



- μ has little effect on stiffness at the no pressure state or M3E3
 - Stiffness and stiffness ratio increase significantly with μ at intermediate pressure states
 - Maximum stiffness ratios are almost the same for all friction coefficient cases

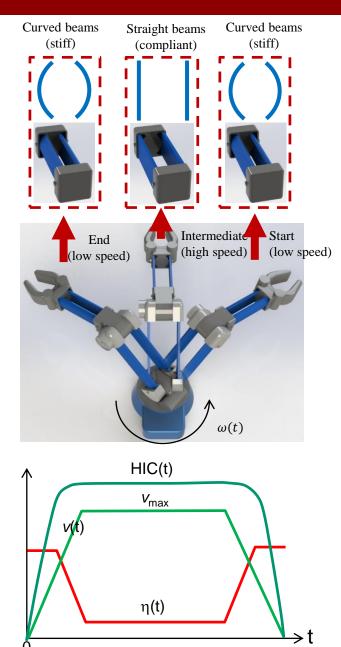
Number of laminates (n)

- Same total thickness for all cases: 15.9 mm
- The more number of laminates, the higher the stiffness ratio
- The less number of laminates, the higher the stiffness range



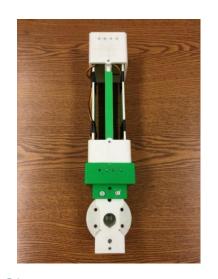
Compliant Links for Corobots

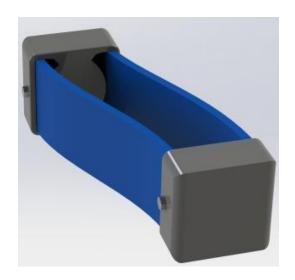
- Stiffness control theme: high stiffness at low speed, low stiffness at high speed
- Keep safety level below a threshold
- Under the safety constraint, the higher the stiffness of the robot link, the better of the control performance

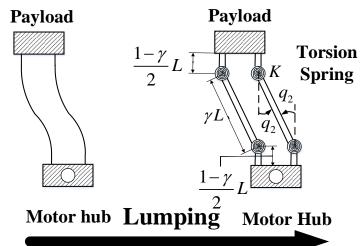


Dynamics Control of Variable Stiffness Link (1)

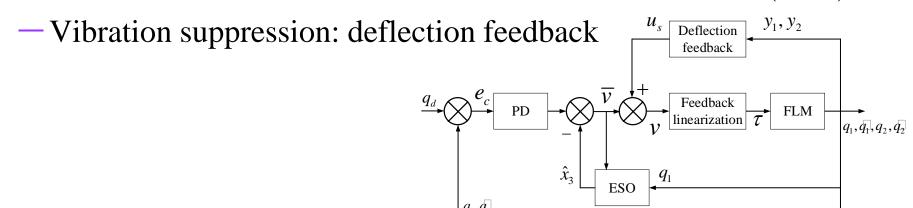
Dynamic Modeling: the pseudo-rigid-body model







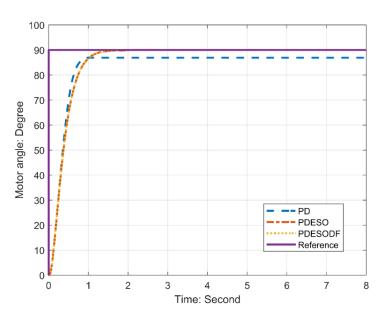
- Compound control architecture
 - Uncertainties and disturbances: extended state observer (ESO)

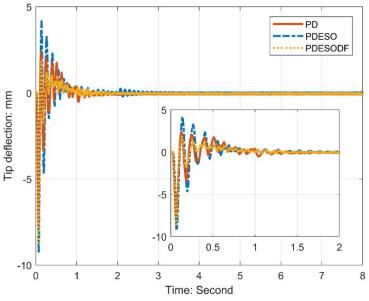


Dynamics Control of Variable Stiffness Link (2)

 Smaller steady-state error (by uncertainties and disturbance compensation)

 Better vibration suppression (by deflection feedback)





Impact Dynamics of Variable Stiffness Link

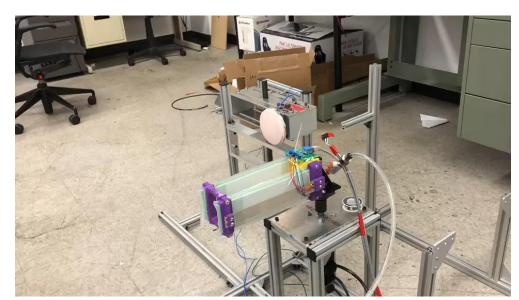
A mass-spring-mass impact model

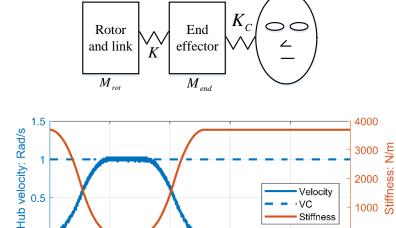
• Single-link case (by optimal control):

Low-speed: high stiffness

—High-speed: low stiffness

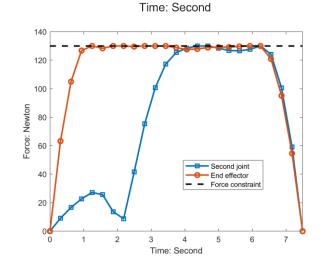
Multi-link case (by optimization)





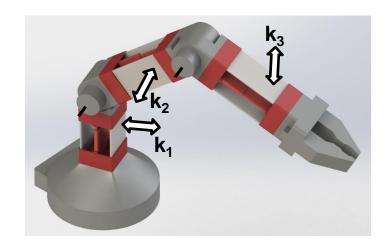
 M_{H}

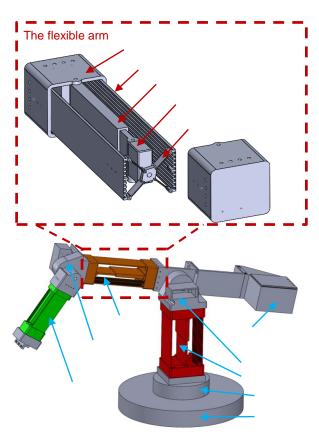
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Future Work

- Methods for simultaneously controlling motion and stiffness for achieving maximum performance under safety constraints, and
- Design, stiffness and motion control of multi-linked robotic manipulators with variable stiffness arms





Publications

- 1. She, Y., Meng, D., Su, H.-J., Song, S, and Wang, J. "Introducing mass parameters to Pseudo–Rigid–Body models for precisely predicting dynamics of compliant mechanisms". Mechanism and Machine Theory, 2018, 126: 273-294.
- 2. She, Y., Su, H.-J., Meng, D., Song, S, and Wang, J. "Design and Modeling of a Compliant Link for Inherently Safe Corobots", ASME Journal of Mechanisms and Robotics. 2018; 10(1):011001 -011001-10.
- 3. She, Y., Song, S., Su, H.-J., and Wang, J. "Compliant joint or compliant link to address safety for physical human-robot interaction", The International Journal of Robotics Research, under review.
- 4. She, Y., Su, H.-J., Meng, D., and Lai C. "Design and Modeling of a Continuously Tunable Stiffness Arm for Safe Human-Robot Interaction", ASME Journal of Mechanisms and Robotics, under review.
- 5. T. Morrison, S. Member, C. Li, X. Pei, and H. Su, "A Novel Rotating Beam Link for Variable Stiffness Robotic Arms," submitted to IEEE Robot. Autom. Lett., 2019.
- 6. Siyang Song, Yu She, Junmin Wang, and Haijun Su, "Control of Parallel-guiding Flexible Link Manipulators Using Pseudo-Rigid Body Model," Submitted to Robotics and Autonomous Systems
- 7. She, Y., Meng, D., Cui, J. and Su, H.-J., "On the Impact Force of Human-Robot Interaction: Joint Compliance vs. Link Compliance." In: *Proceedings of IEEE 2017 International Conference on Robotics and Automation* (ICRA 2017). May 28-June 3, 2017. Singapore. (2017).
- 8. She, Y., Meng, D. and Su, H.-J., "Pseudo-Rigid-Body Models for Dynamics of Compliant Robotic Links." In: *Proceedings of ASME 2017 International Design Engineering Technical Conferences*. Cleveland, OH. (2017): DETC2017- 67949.
- 9. She, Y., Su, H.-J., Lai, C. and Meng, D, "Design and Prototype of a Tunable Stiffness Arm for Safe Human-Robot Interaction." In: Proceedings of ASME 2016 International Design Engineering Technical Conferences. Charlotte, NC. (2016): DETC2016-59523.
- 10. Siyang Song, Yu She, Junmin Wang, and Haijun Su, "Barrier Lyapunov Function Based Control of a Flexible Link CoRobot with Safety Constraints," Proceedings of the ASME 2018 Dynamic Systems and Control Conference, 2018. **Best paper award.**
- 11. R. Hu, V. Venkiteswaran and H.-J. Su, "A Variable Stiffness Robotic Arm Using Linearly Actuated Compliant Parallel Guided Mechanism", Proceedings of 4th IFToMM Symposium on Mechanism Design for Robotics, September 11th 13th, 2018, Udine, Italy.
- 12. Zeng, Xianpai., Su, H.-J., "Design, Modeling and Experiment of a Parallel-guided Robotic Arm with Variable Stiffness through Layer Jamming" in preparation
- 13. Siyang Song, Xianpai Zeng, Yu She, Junmin Wang and Haijun Su, "Modeling and Control for Inherent Safe Robots with Variable Stiffness Link (VSL)" in preparation
- 14. Yitong Zhou, "Discrete Layer Jamming for Safe Co-Robots" in preparation
- 15. Yitong Zhou, "Discrete Layer Jamming for Variable Stiffness Co-Robot Arms" in preparation