

# Symmetries in Nonlinear Cyber-Physical Systems for Compositionality

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# Introduction and Motivation

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- Overall goal: results for system integration through compositionality.
- Compositionality: system-level properties can be computed from local properties of components
  - System-level properties *preserved* when expanding system.
- Initial focus: invariant properties for symmetric systems.
- Emphasis on general results, not limited to specific system dynamics.
- Initial results: symmetric systems and stability.
- These results are Lyapunov-based, so the natural extension is to passivity.
- Also working toward use of *approximate* symmetries.
- [9, 12, 10, 11, 14, 13, 4, 19]

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- Nonlinear Symmetric Systems and Compositionality
- Nonlinear Compositional Stability Results ( $V$ -based)
  - stability for “growing” systems
  - robustness for “shrinking” and failing systems
- Optimal Control for Nonlinear Symmetric Systems
- Mechanical Cyber-Physical Systems
- Ongoing and Future work

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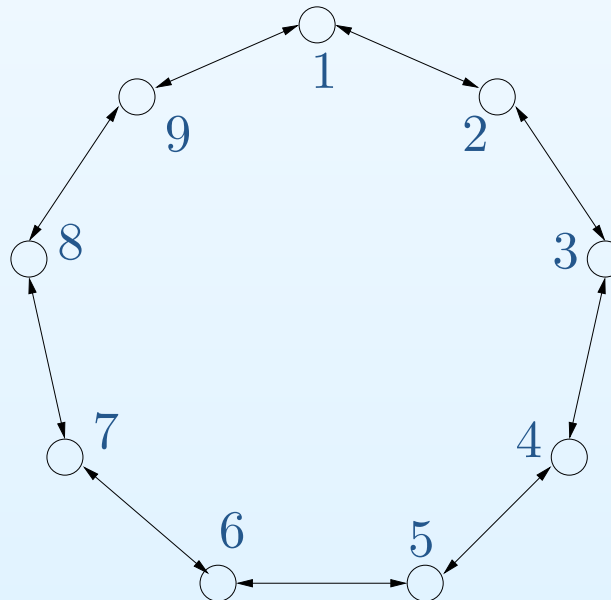
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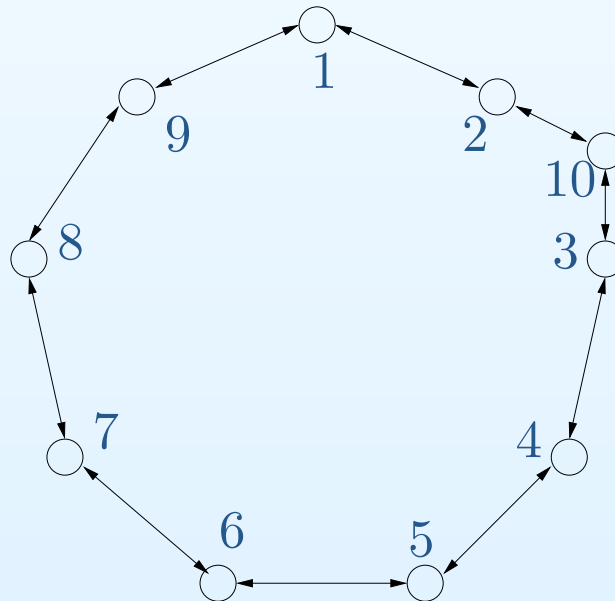
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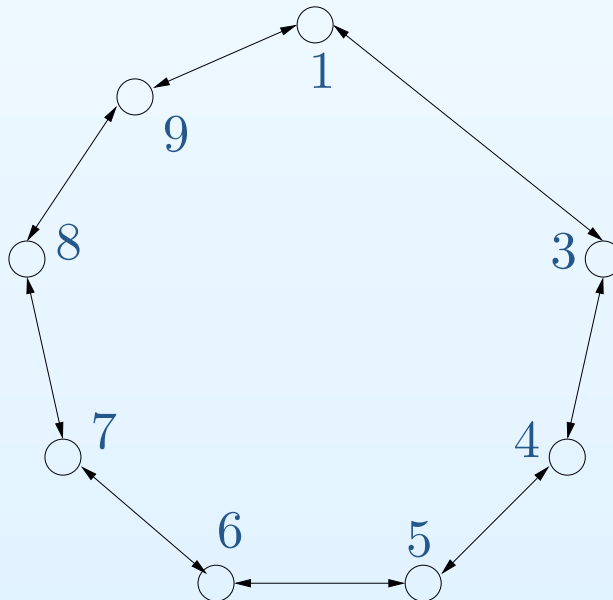
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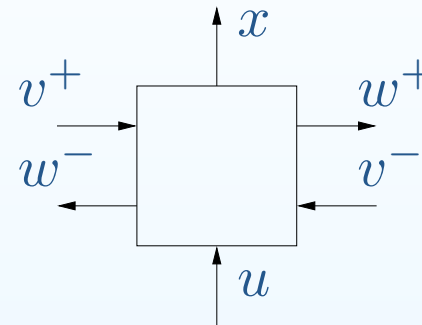
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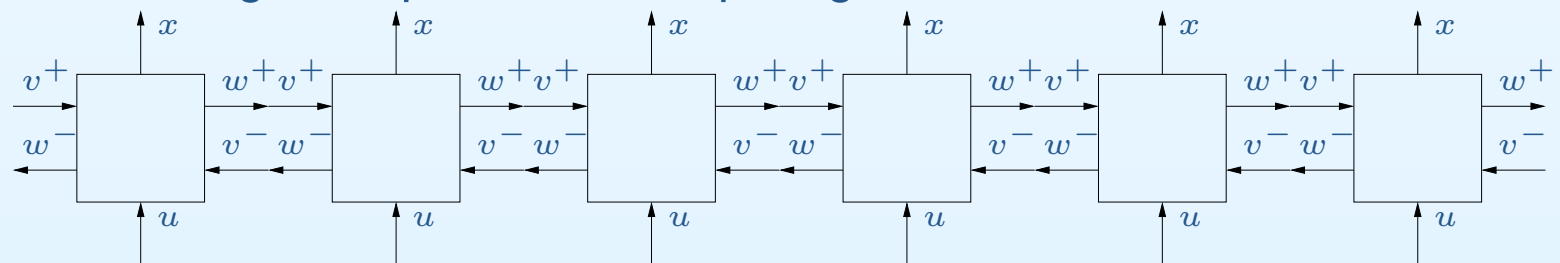
Consider a *basic building block element*:



where

- $x$  is the state vector;
- $u$  is the vector of control inputs;
- $w^\pm$  are the *outputs*; and,
- $v^\pm$  are the coupling inputs.

Connecting the inputs to the outputs gives



# Periodic Interconnections

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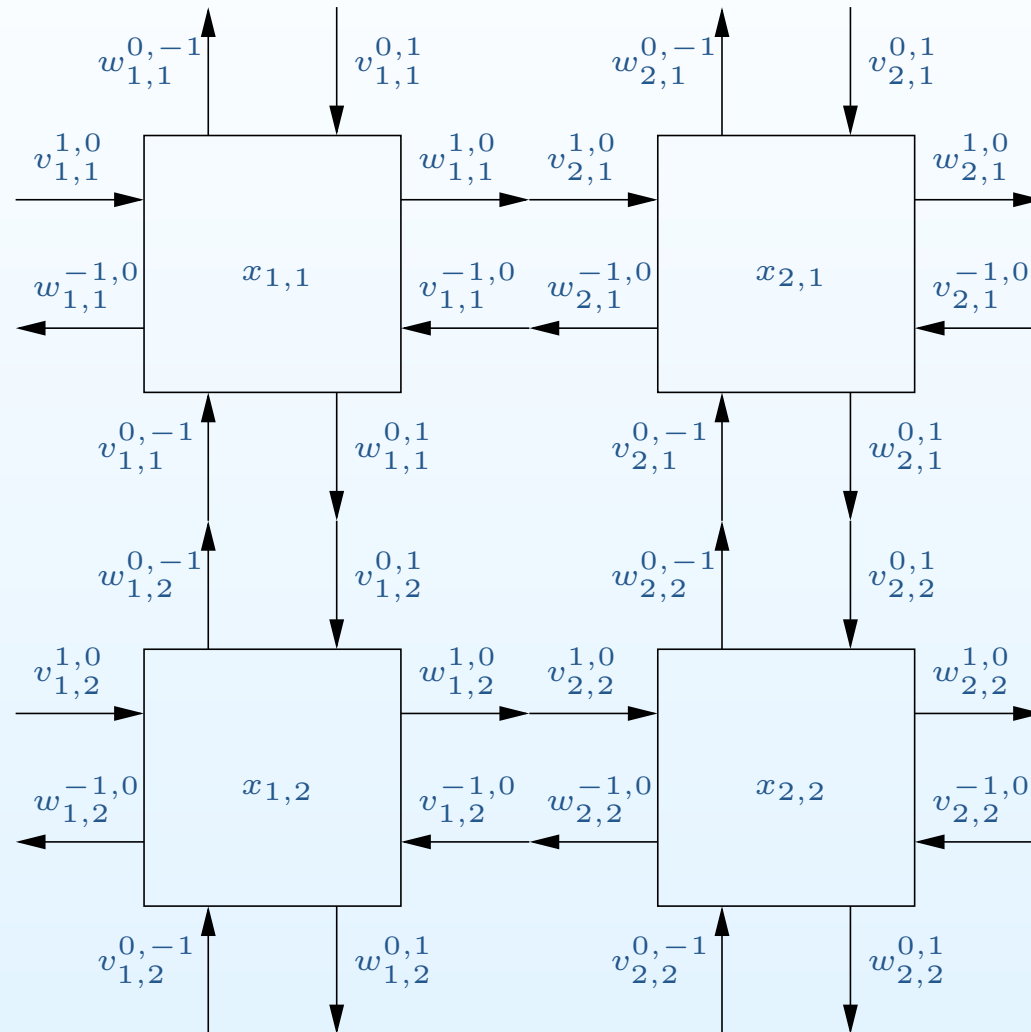
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Systems can be built with various topologies:





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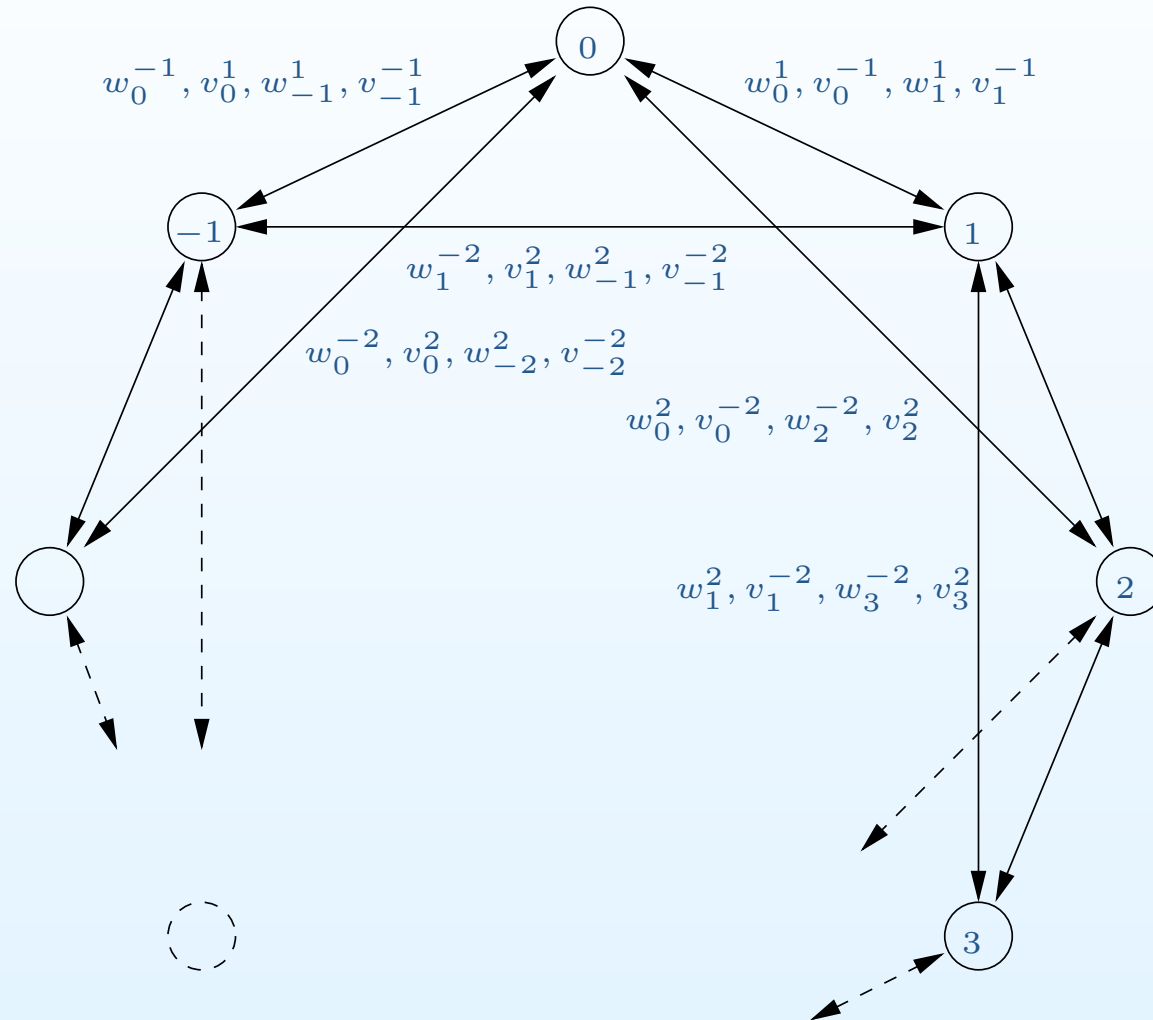
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# Group and Graph Theory Representation

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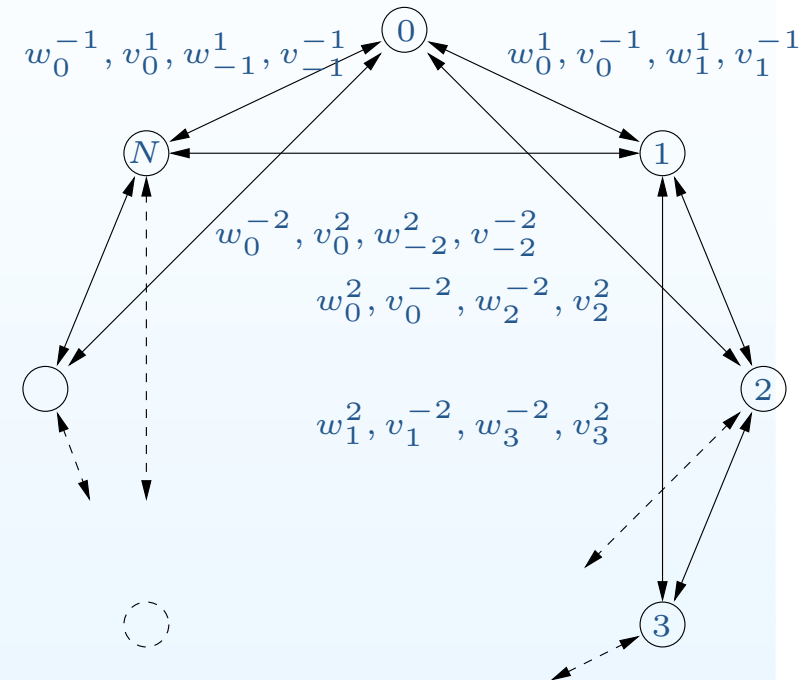
## Optimal Control of Symmetric Systems

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- Represent connectedness with *generators*,  $\{s_1, \dots, s_n\}$  with  $g_2 = s_i g_1$ .
- *Cayley Graph*:
  - nodes = components
  - edges = communication
- *Equivalent connections* for two systems if they have the same generators.
- Example:  $S = \{-2, -1, 1, 2\}$ .
- Each component:

$$\dot{x}_i = f_i(x) + g_i(x)u$$

$$w_i^s(t) = w_i^s(x_i(t)).$$



- Periodic interconnections:

$$v_g^s(t) = w_{s-1g}^s(x_{s-1g}(t))$$

$$w_g^s(t) = v_{sg}^s(x_g(t))$$

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A *symmetric system* has components with identical dynamics:

$$f_{g_1}(x) = f_{g_2}(x), g_{g_1,j}(x) = g_{g_2,j}(x), w_{s^{-1}g_1}^s(x) = w_{s^{-1}g_2}^s(x)$$

and identical control laws

$$u_{g_1,j} \left( x_1(t), w_{s_1^{-1}g_1}^{s_1} (x_2(t)), \dots, w_{s_{|X|}^{-1}g_1}^{s_{|X|}} (x_{|X|+1}(t)) \right) =$$
$$u_{g_2,j} \left( x_1(t), w_{s_1^{-1}g_2}^{s_1} (x_2(t)), \dots, w_{s_{|X|}^{-1}g_2}^{s_{|X|}} (x_{|X|+1}(t)) \right)$$

for all  $g_1 \in G_1, g_2 \in G_2, s \in X, x \in \mathbb{R}^n,$

$(x_1, x_2, \dots, x_{|X|+1}) \in \mathbb{R}^n \times \mathbb{R}^n \times \dots \times \mathbb{R}^n$  and  $j \in \{1, \dots, m\}$

where  $m = m_{g_1} = m_{g_2}$ .

Two systems are *equivalent* if they are both symmetric with equal components and the *same generators*.

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- **Stability:** if a symmetric distributed system is stable, so is any equivalent symmetric system, so can “grow” or “shrink.”
  - Growing: useful for analysis/design on a small system with guaranteed invariance for larger equivalent systems
  - Shrinking: reconfigurable robustness
- **Robustness:** stability in the sense of Lyapunov is guaranteed even when components fail without any reconfiguration necessary.
- Requires a symmetric Lyapunov function:  $V = \sum_{i \in G} V_i$  where

$$V_{g_1} \left( x_1, w_{s_1^{-1}g_1}^{s_1} (x_2), \dots, w_{s_{|X|}^{-1}g_1}^{s_{|X|}} (x_{|X|+1}) \right) =$$
$$V_{g_2} \left( x_1, w_{s_1^{-1}g_2}^{s_1} (x_2), \dots, w_{s_{|X|}^{-1}g_2}^{s_{|X|}} (x_{|X|+1}) \right)$$

for all  $g_1, g_2 \in G$  and  $(x_1, x_2, \dots, x_{|X|+1}) \in \mathbb{R}^n \times \dots \times \mathbb{R}^n$ .

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- From [18] second-order mechanical system agents:

$$\frac{d}{dt} \begin{bmatrix} x_i \\ \dot{x}_i \\ y_i \\ \dot{y}_i \end{bmatrix} = \begin{bmatrix} \dot{x}_i \\ 0 \\ \dot{y}_i \\ 0 \end{bmatrix} + \begin{bmatrix} 0 \\ 1 \\ 0 \\ 0 \end{bmatrix} u_{i,1} + \begin{bmatrix} 0 \\ 0 \\ 0 \\ 1 \end{bmatrix} u_{i,2}. \quad (1)$$

- Goal= regular  $(N + 1)$ -polygon centered at the origin, hence

$$d_{ij} = \begin{cases} 1, & |i - j| = 1 \\ \frac{\sin(\frac{2\pi}{N+1})}{\sin(\frac{\pi}{N+1})}, & |i - j| = 2 \end{cases} \quad \text{and} \quad r_i = \frac{1}{2 \sin \frac{\pi}{N}}.$$

- Take the control law to be  $u =$

$$-\sum_j \begin{bmatrix} \frac{(\sqrt{(x_i-x_j)^2+(y_i-y_j)^2}-d_{ij})}{\sqrt{(x_i-x_j)^2+(y_i-y_j)^2}} (x_i - x_j) \\ \frac{(\sqrt{(x_i-x_j)^2+(y_i-y_j)^2}-d_{ij})}{\sqrt{(x_i-x_j)^2+(y_i-y_j)^2}} (y_i - y_j) \end{bmatrix} - k_d \begin{bmatrix} \dot{x}_i \\ \dot{y}_i \end{bmatrix} - \begin{bmatrix} \frac{\sqrt{x_i^2+y_i^2}-r_i}{\sqrt{x_i^2+y_i^2}} x_i \\ \frac{\sqrt{x_i^2+y_i^2}-r_i}{\sqrt{x_i^2+y_i^2}} y_i \end{bmatrix}.$$

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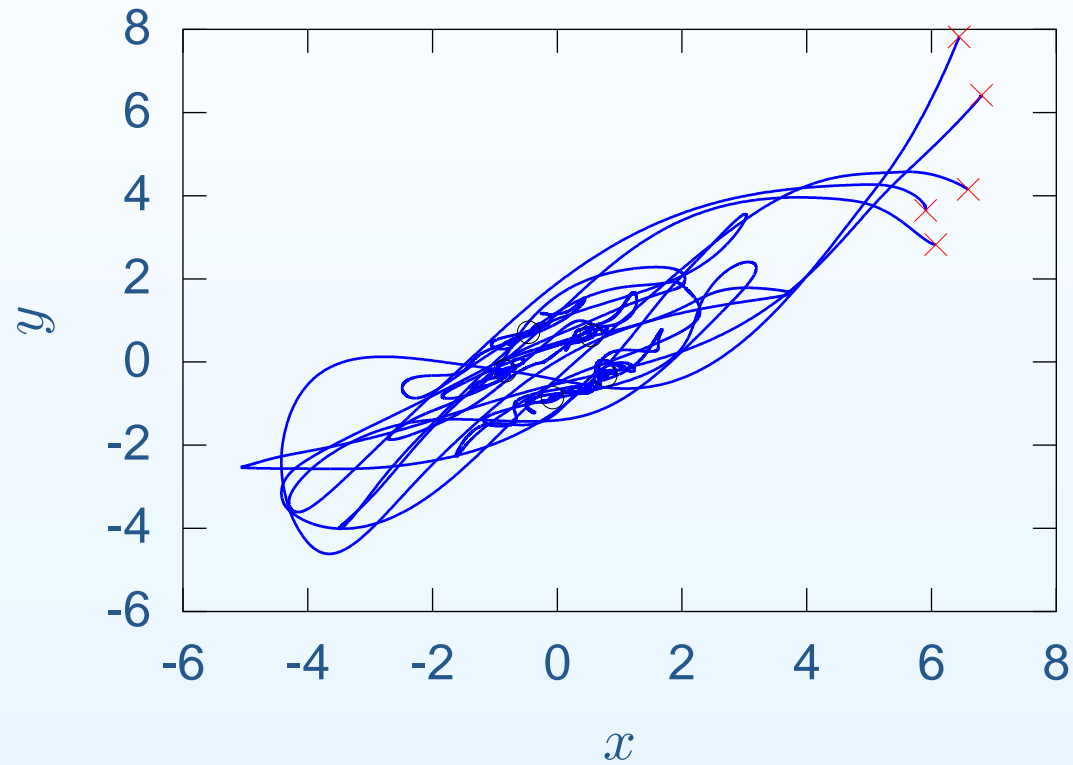
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Five robot stable formation control.

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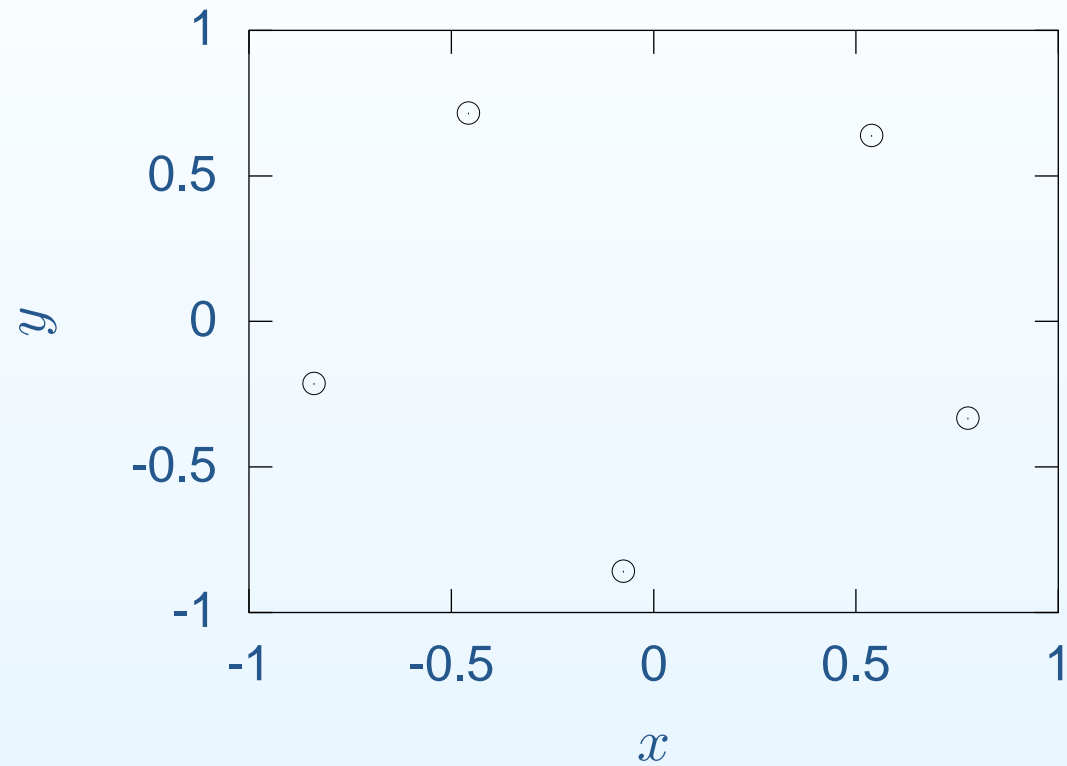
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Initial and final configurations.

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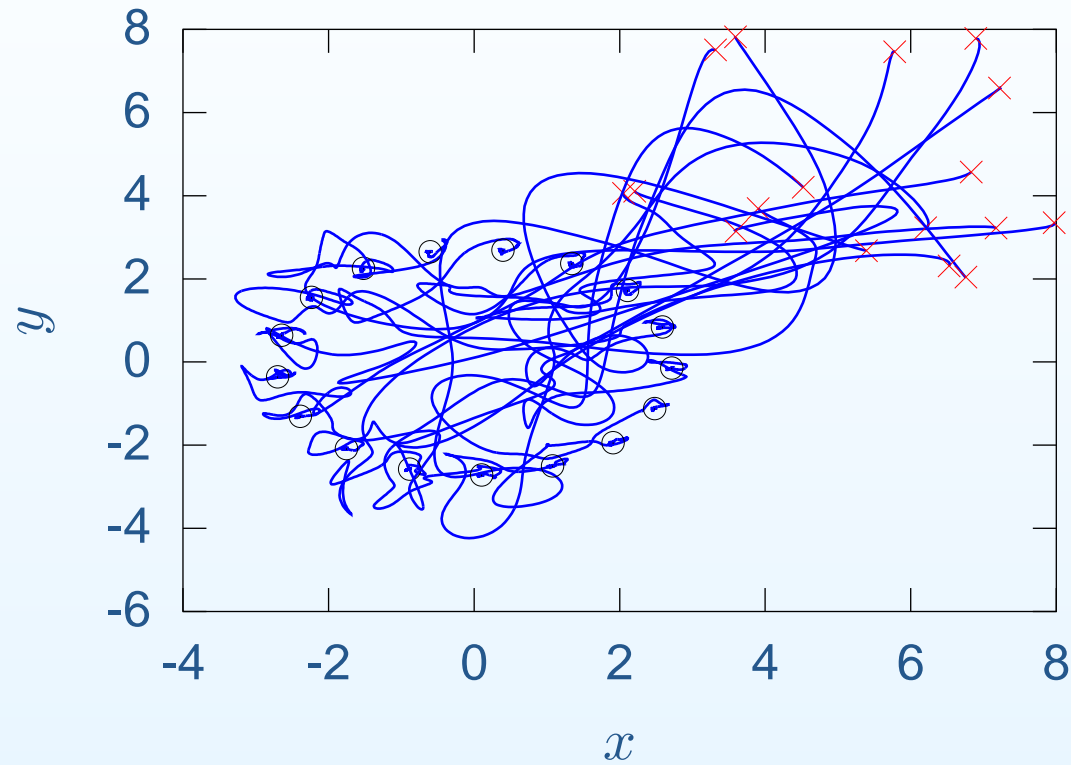
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Seventeen-agent formation control.



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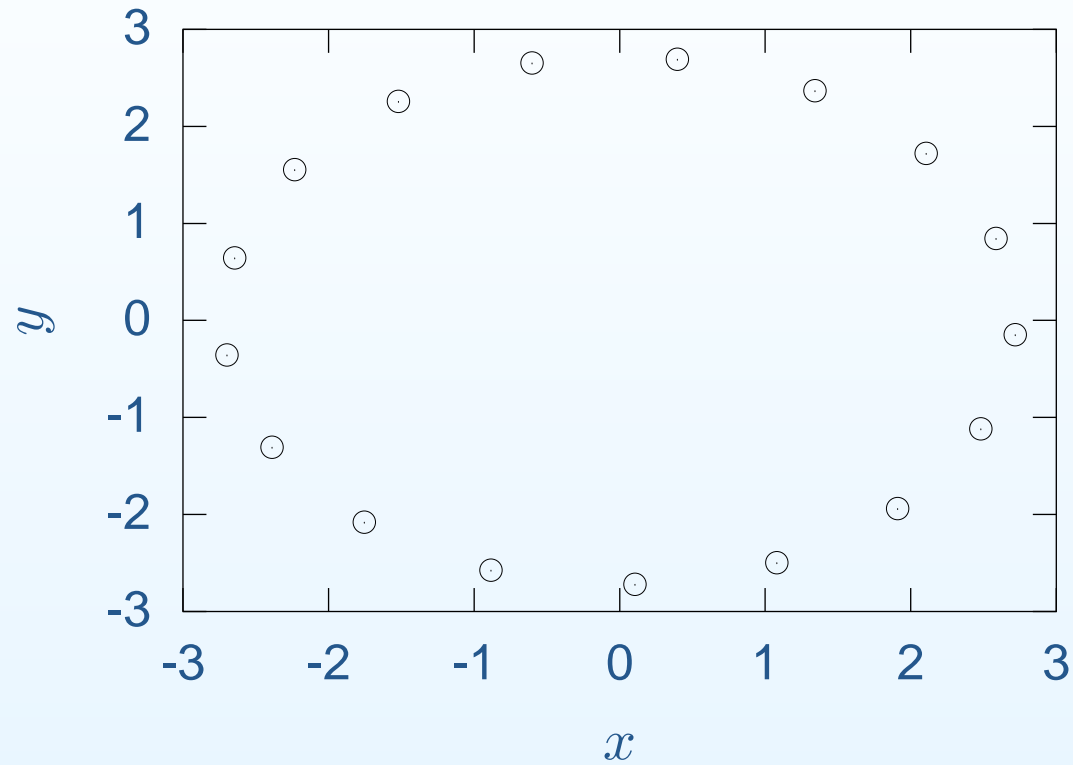
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Starting and ending configurations.

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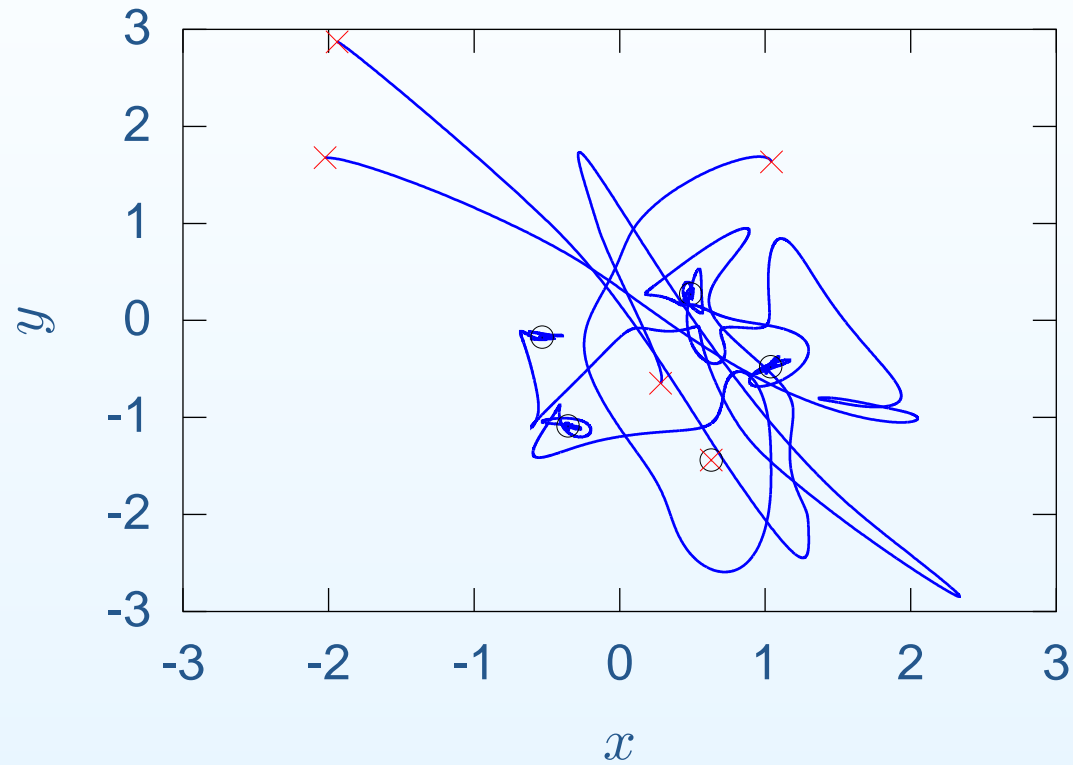
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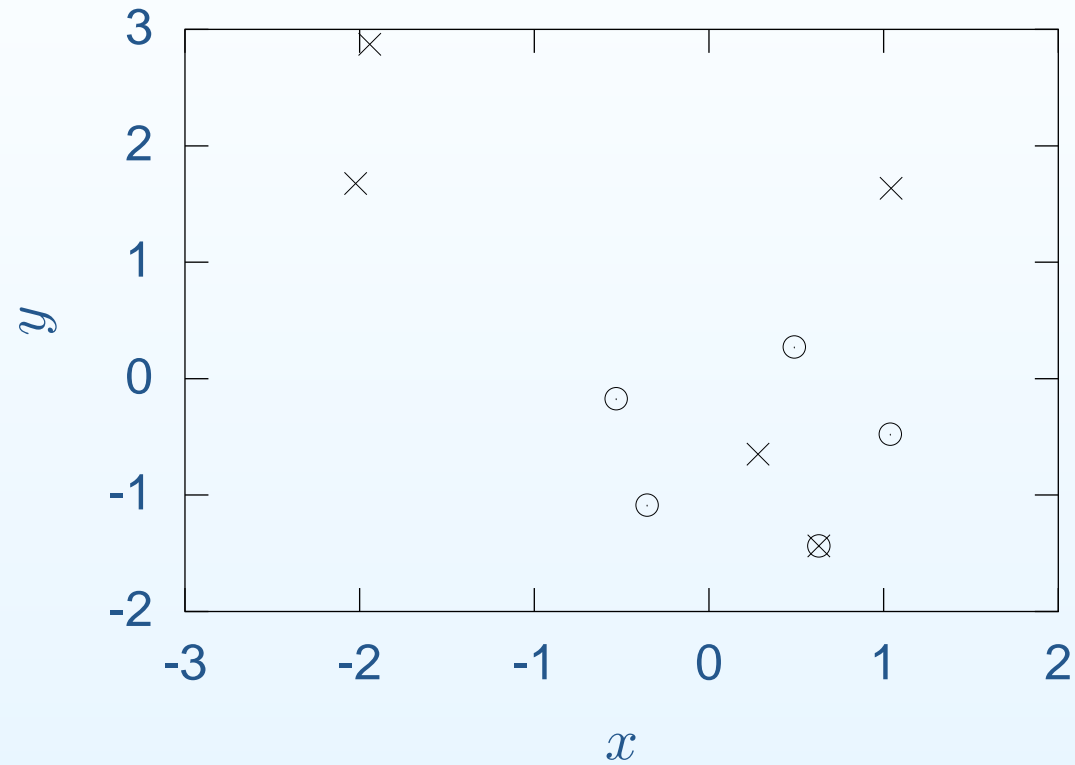
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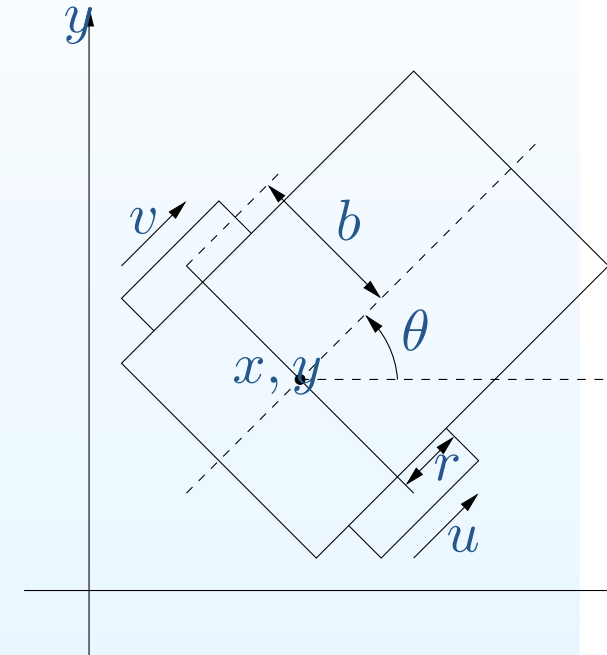
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We are investigating the effect of approximate symmetries and symmetry-breaking by looking at optimal formation control. Minimize control effort and deviation from desired formation

$$\begin{aligned}
 J = & \int_0^{t_f} \left[ \frac{1}{2} \sum_{i=1}^n u_i^2 + v_i^2 \right. \\
 & + \sum_{i=1}^n \left[ \lambda_{x_i} \left( \dot{x}_i - \frac{r}{2} \cos \theta_i (u_i + v_i) \right) \right. \\
 & + \lambda_{y_i} \left( \dot{y}_i - \frac{r}{2} \sin \theta_i (u_i + v_i) \right) \\
 & \left. \left. + \lambda_{\theta_i} \left( \dot{\theta}_i - \frac{r}{2b} (u_i - v_i) \right) \right] \right. \\
 & \left. + k \sum_{i=1}^{n-1} (d_{i,i+1} - \tilde{d})^2 \right] dt
 \end{aligned}$$



Consider  $k \in [0, +\infty)$ .

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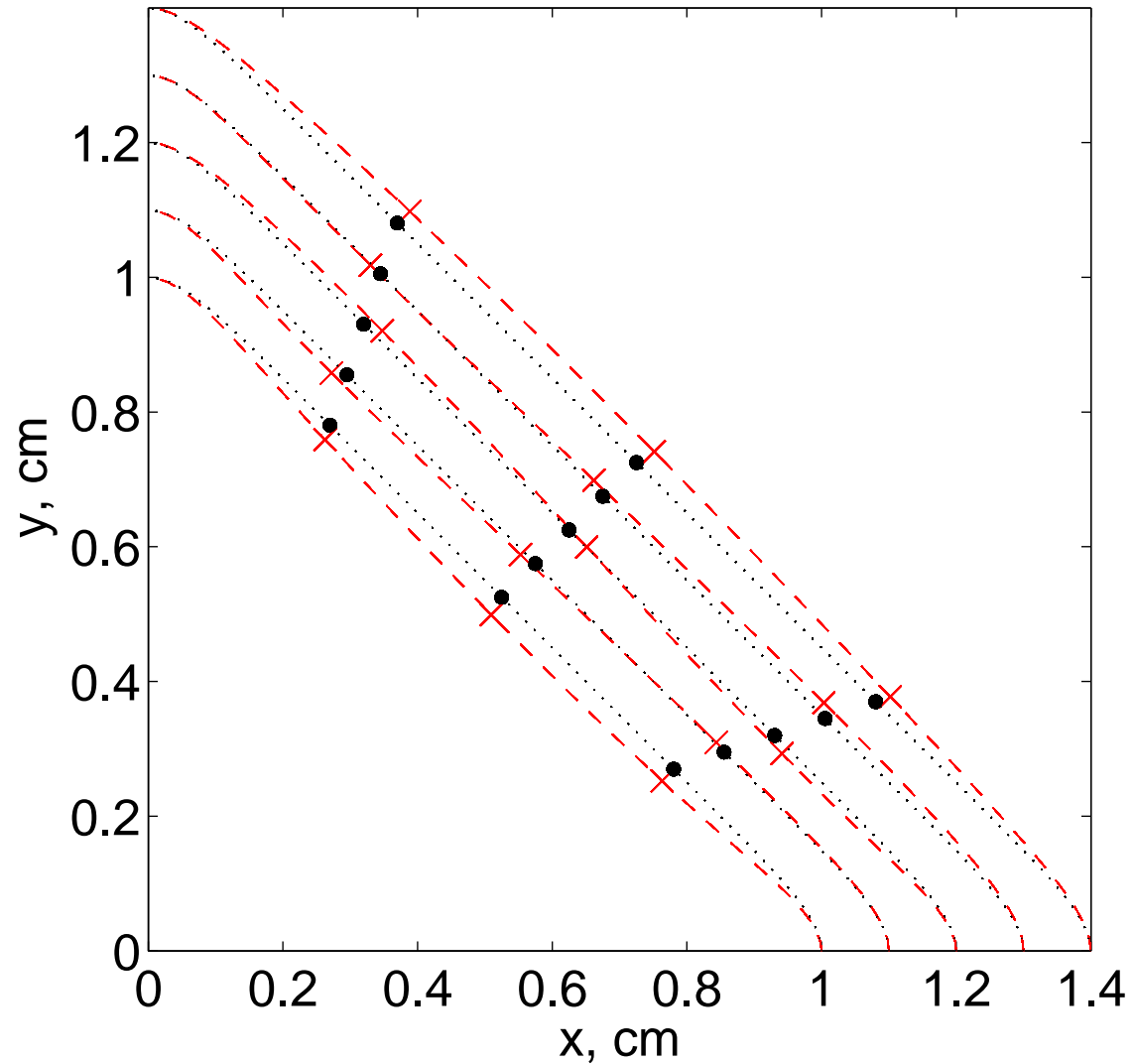
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Solutions:



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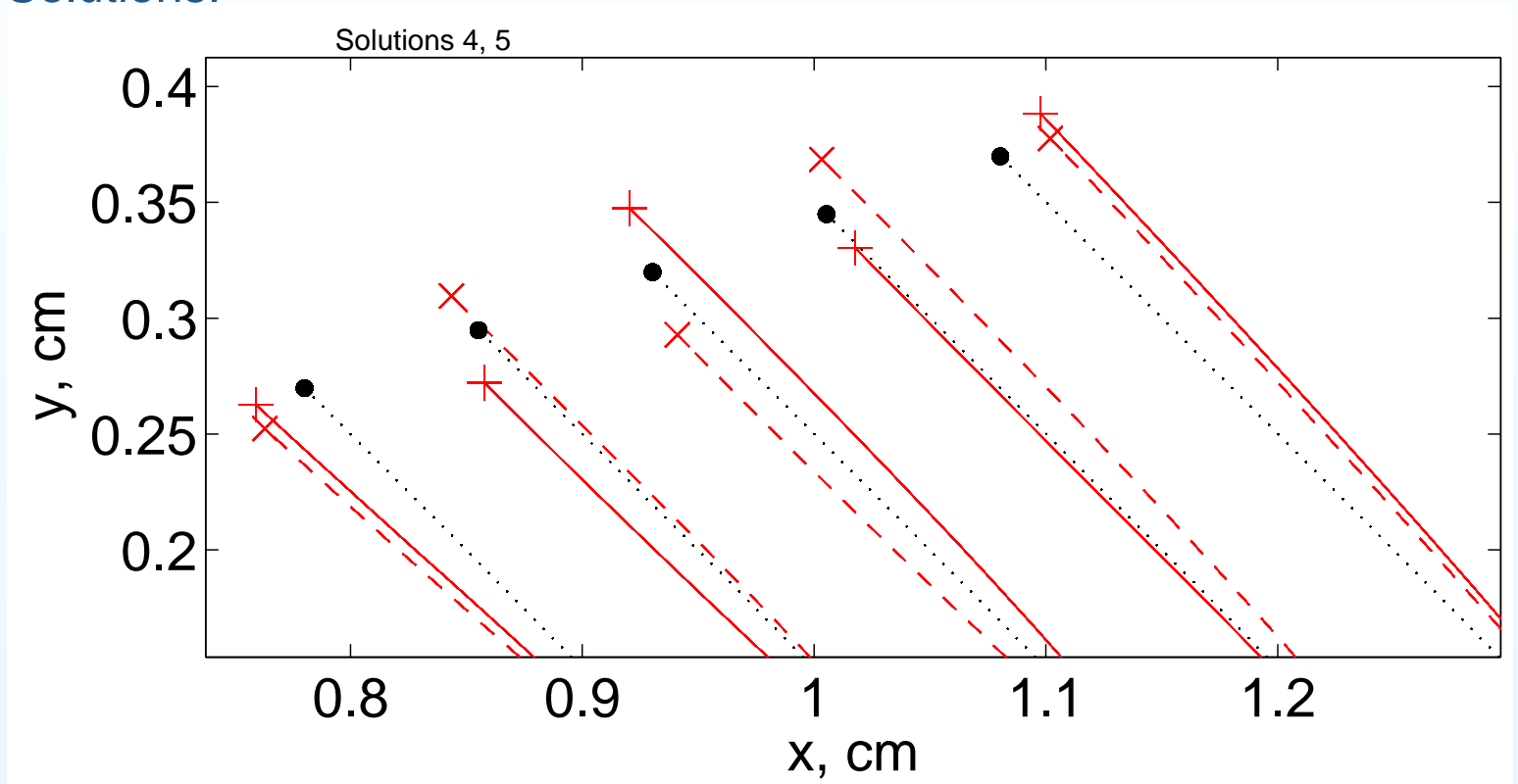
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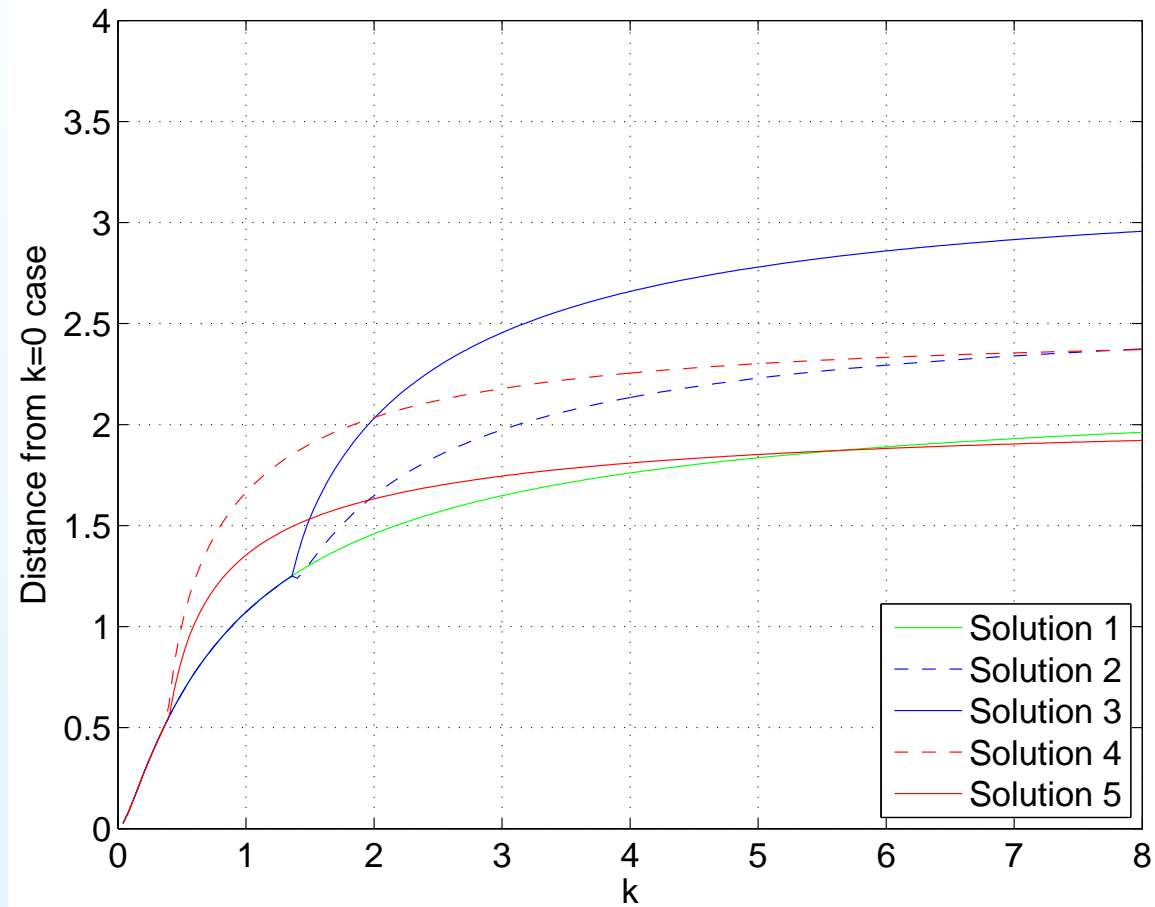
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Bifurcating solutions:



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## Main Results:

- Existence of multiple solutions
  - Limiting cases:  $k = 0$  and  $k \rightarrow \infty$ .
  - Characterization of bifurcations.
- For holonomic system: solutions *and* bifurcations must be symmetric [5, 6].
- For nonholonomic system: symmetry is broken by agent itself
  - Bifurcations have small deviations
  - On the order of the wheelbase vs. path length
  - Further investigation: to give insight into full range of approximate systems.



# Control of *Mechanical* Systems

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- Control + Mechanical = Cyber + Physical
- Instead of generic

$$\dot{x} = f(x) + g(x)u$$

consider the case where the vector fields *came from* a first principle, i.e., Lagrange's equations.

- For  $\Sigma = (M, \mathbb{G}, \{Y_1, \dots, Y_m\}, U)$  the equations of motion are

$$\dot{x}^i = v^i$$

$$\dot{v}^i = -\Gamma_{jk}^i v^j v^k + u^a Y_a^i.$$

- Very difficult open questions concerning control away from equilibrium points. E.g., only sufficient conditions for controllability.
- Approach: decompose velocities into actuated and unactuated degrees of freedom and study the coupling between them.

# Mechanical System Velocity Decomposition

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- Decompose the velocity curve,  $\dot{\gamma}(t)$  of  $\Sigma$  into

$$\dot{\gamma}(t) = w^a(t)X_a(\gamma(t)) + s^b X_b^\perp(\gamma(t)).$$

- From Lagrange's equations, it follows that

$$\dot{s}^b(t) = -\hat{\Gamma}_{ap}^b w^a w^p - 2\hat{\Gamma}_{ar}^b w^a s^r - \hat{\gamma}_{rk}^b s^r s^k.$$

- Direct control over the  $w$ s, therefore the vector-valued quadratic form  $\hat{\Gamma}_{ap}^b w^a w^p$  plays a key role in control.
  - If it is indefinite, can both increase and decrease  $s$ , therefore can control all velocities.
  - If positive (negative) definite with other forms zero, can only increase (decrease)  $s$  (roller-racer).

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Main results:

- Stopping (analysis at non-zero velocity) and stopping *algorithms*.
- Strongest algorithms for underactuated by one.
- Controllability computational simplicity.
- Focus is on *coupling dynamics* between actuated and unactuated degrees of freedom.
- Natural extension to system integration and coupling between components.
- References: [7, 15, 16, 17] and related work: [1, 3, 2, 20, 8, 21].

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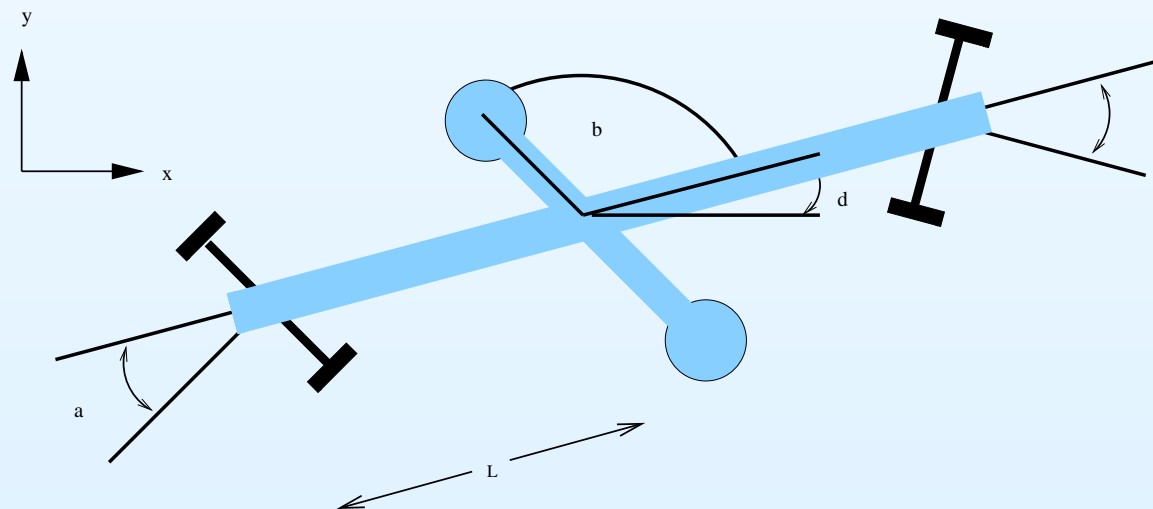
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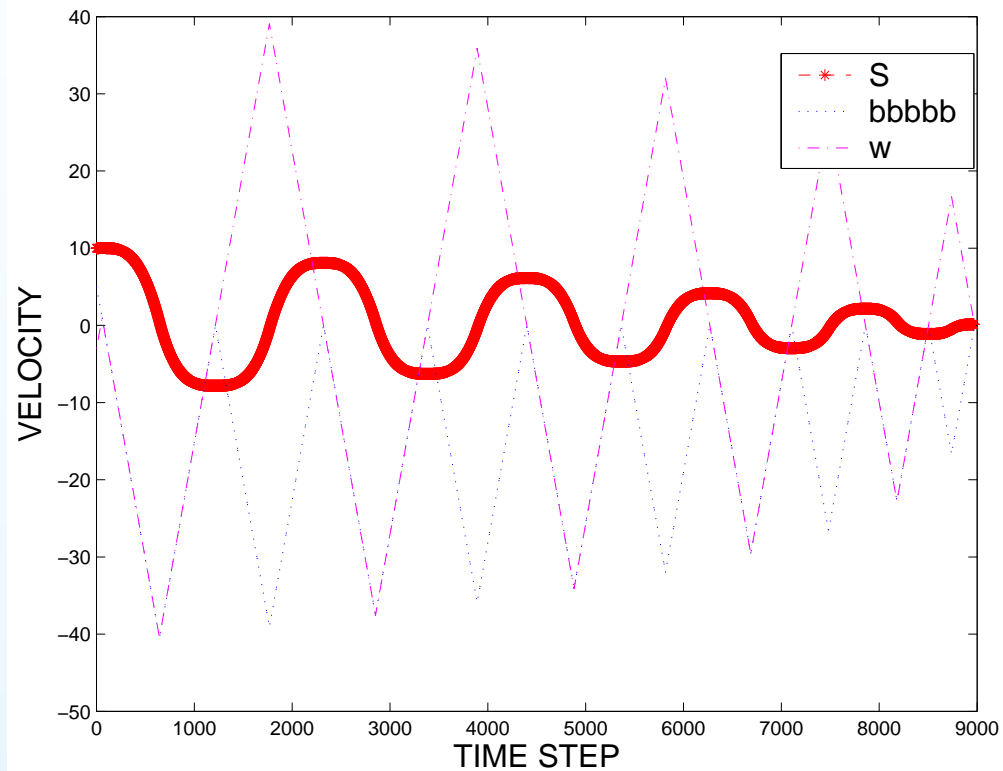
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● [References](#)

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